

24

538815 N91-253384
18P
ND 210491
52-34
13944
P-18

TESTS IN HELIUM ILLUSTRATE HIGH MACH NUMBER INLET - FOREBODY INTERACTIONS

John Weidner and Carl Trexler

NASA Langley Research Center
Hampton, VA 23665-5225

Presented at
1st Workshop on High-Speed Inlet-Forebody Interactions
Sponsored by the JANNAF Airframe integration Panel
January 10, 1991

HIGH-SPEED INLET-FOREBODY INTERACTIONS TESTS

(A Propulsion Perspective)

Objectives:

- Identify the impact of the forebody flow on inlet performance and operability
 - Interaction of thick forebody boundary layer with inlet geometry and compressive shock waves; addressed in current tests
 - Influence of flow uniformity and resulting lateral boundary layer concentrations; not addressed in current tests
- Calibrate/develop CFD codes to allow analysis for other geometries and conditions

HIGH MACH HELIUM TESTS

Langley Mach 18 60" Helium Tunnel

- Why Helium?
 - Ambient total temperature, inexpensive models
 - Large forebody and high Reynolds number match flight conditions
 - Perfect gas, ideal for CFD validation
 - Studies of fundamental shock/viscous interactions to establish performance and operability characteristics. (note: actual inlet configurations cannot be tested due to high value of the ratio of specific heat).
- Helium Test Program
 - Existing sidewall compression inlet models with and without forebody
 - Planned parametric sidewall compression inlet test
 - Parametric 2-D inlet with sidewalls

3-D INLET MODELS

UNCLASSIFIED



30 deg sweep



70 deg sweep

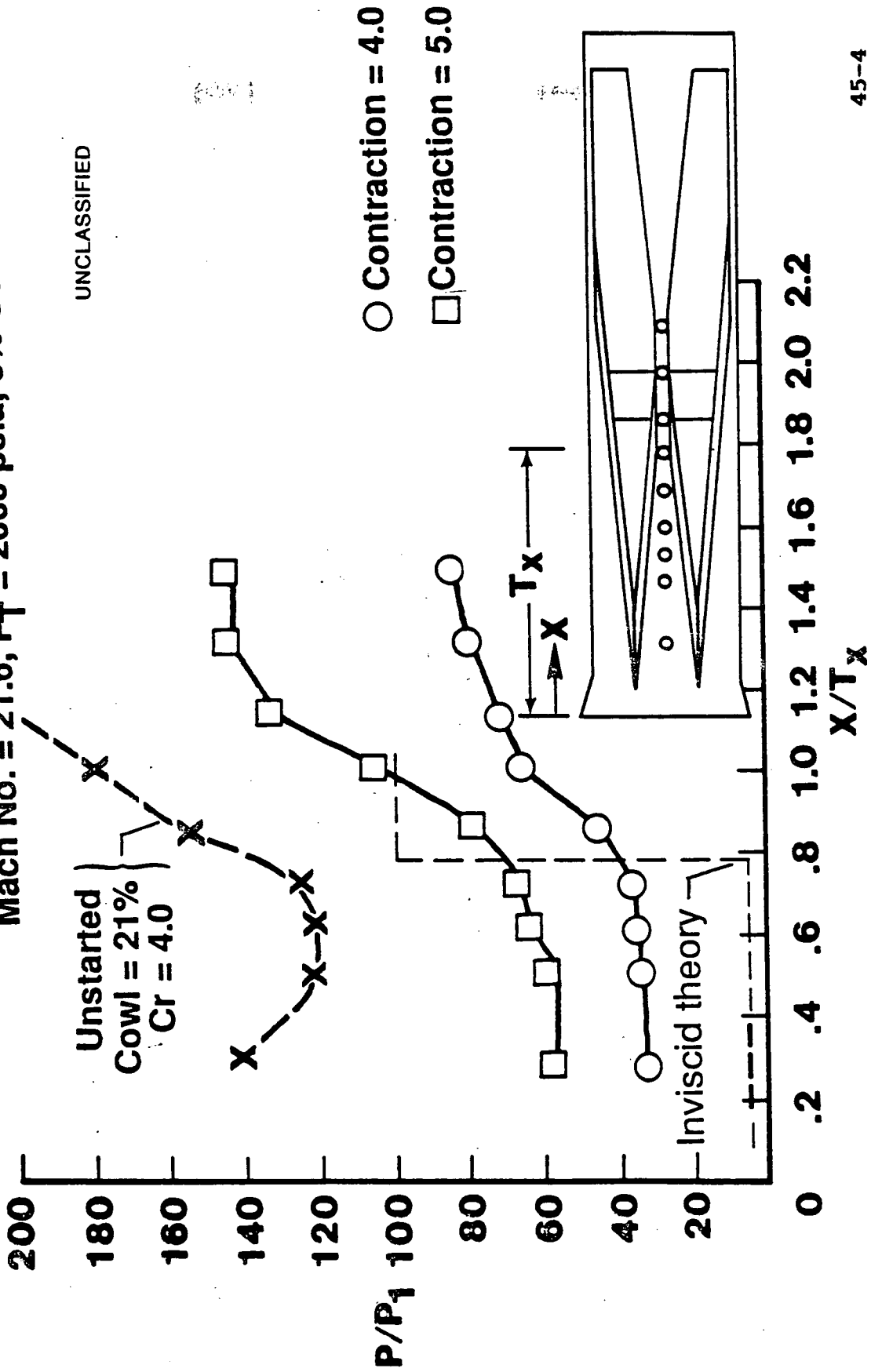
UNCLASSIFIED

ORIGINAL PAGE IS
OF POOR QUALITY

UNCLASSIFIED

30° SWEEP INLET (U) Mach No. = 21.6, $P_T = 2000$ psia, 0% Cowl

UNCLASSIFIED

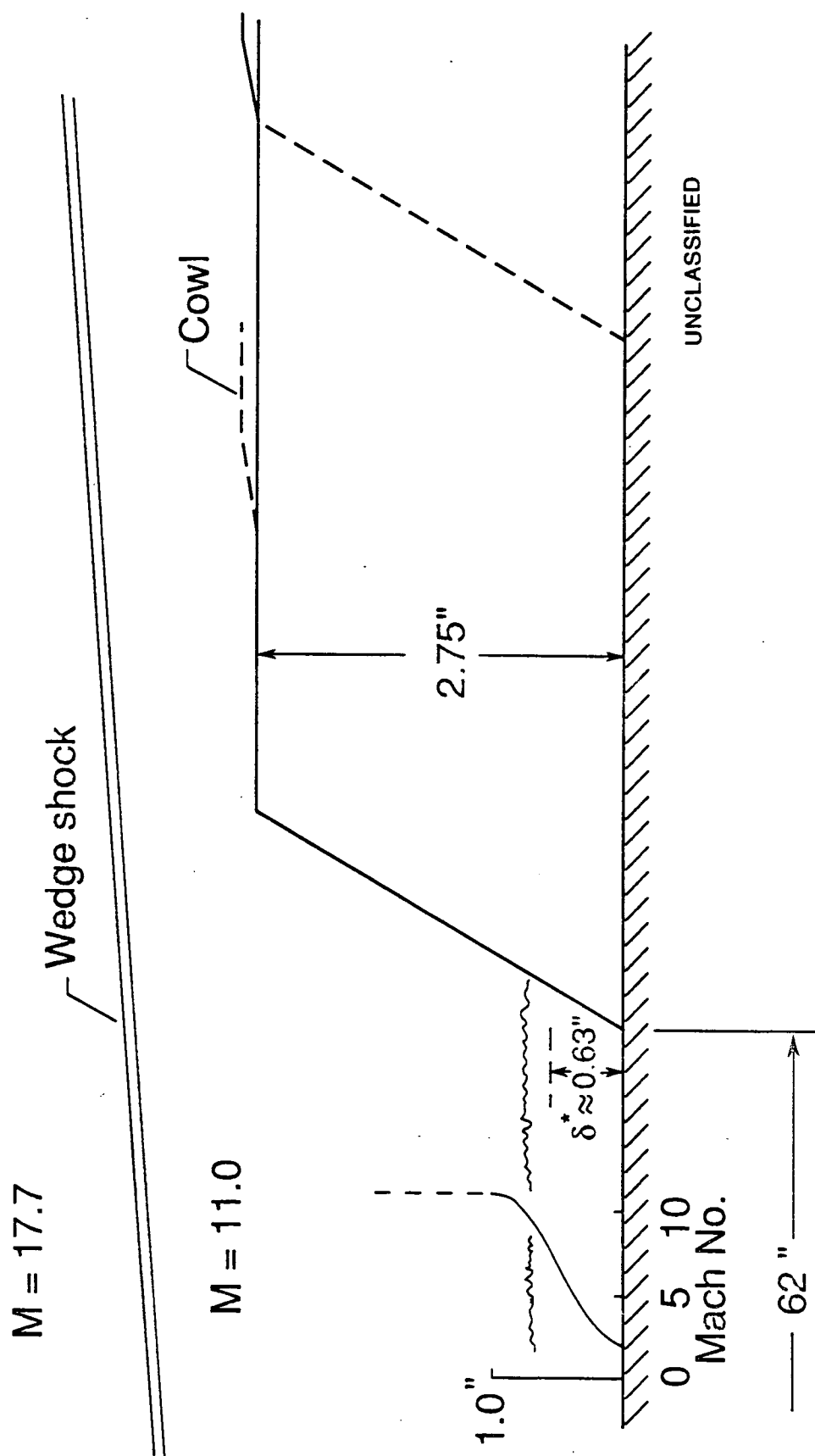


45-4

UNCLASSIFIED

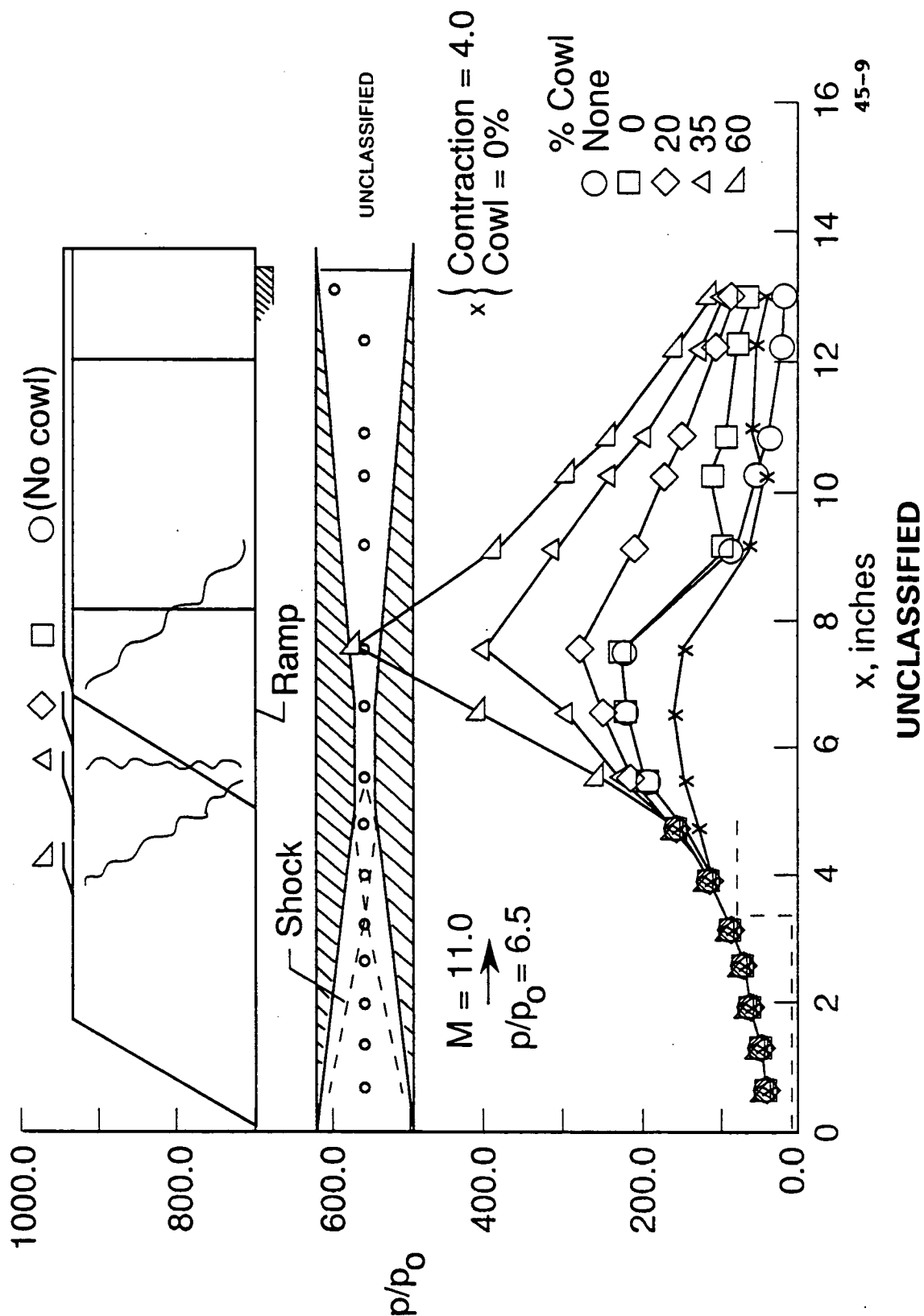
UNCLASSIFIED

BOUNDARY LAYER APPROACHING INLET (U)



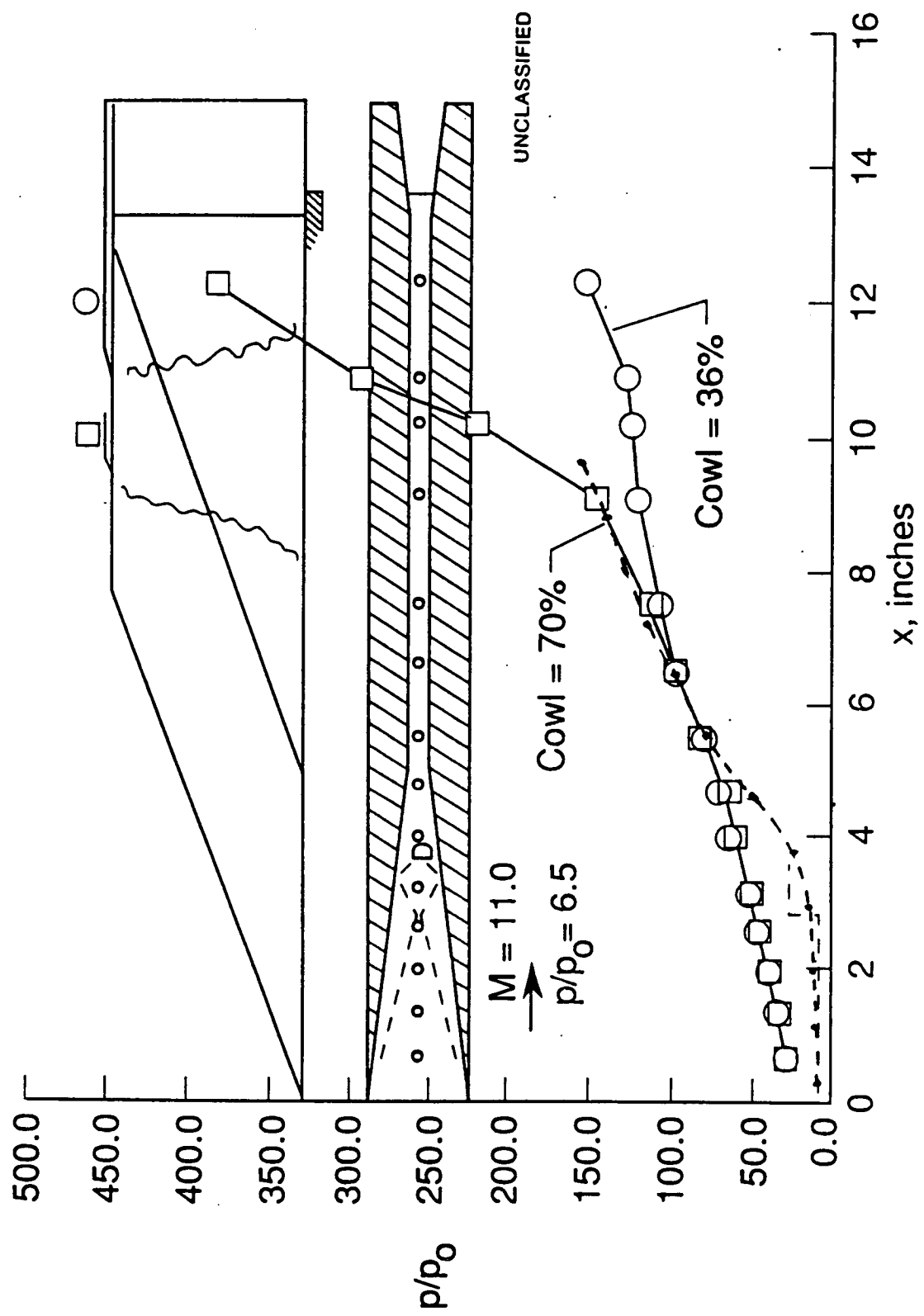
RAMP SURFACE PRESSURE DISTRIBUTION (10)

30° Sweep inlet mounted on 4° wedge foreplate
Mach No. = 18, $P_T = 1200$ psia, $Cr = 5.0$



RAMP SURFACE PRESSURE DISTRIBUTION (U)

70° Sweep inlet mounted on 4° wedge foreplate
Mach No. = 18, $P_T = 1200$ psia, $Cr = 5.0$

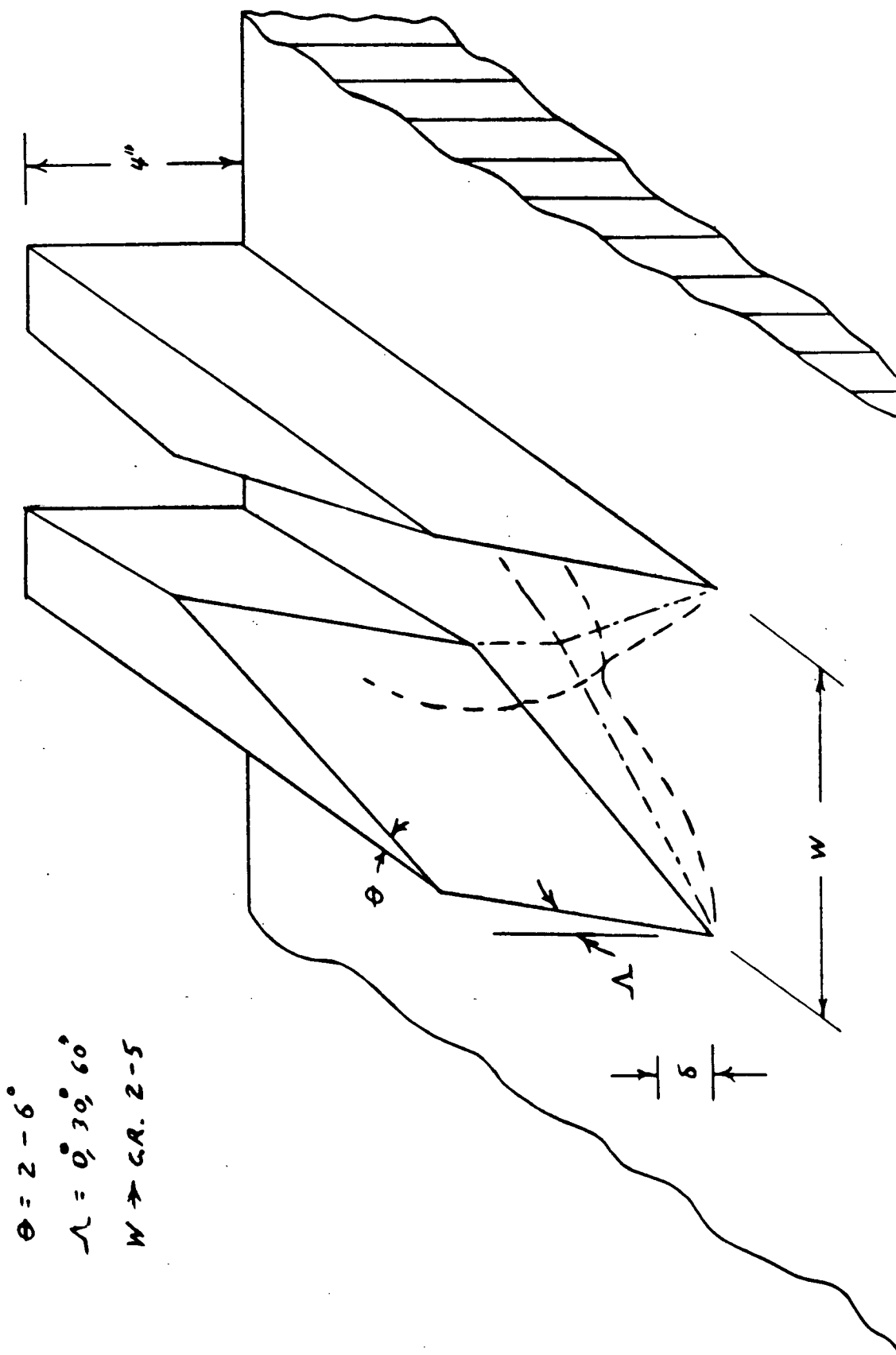


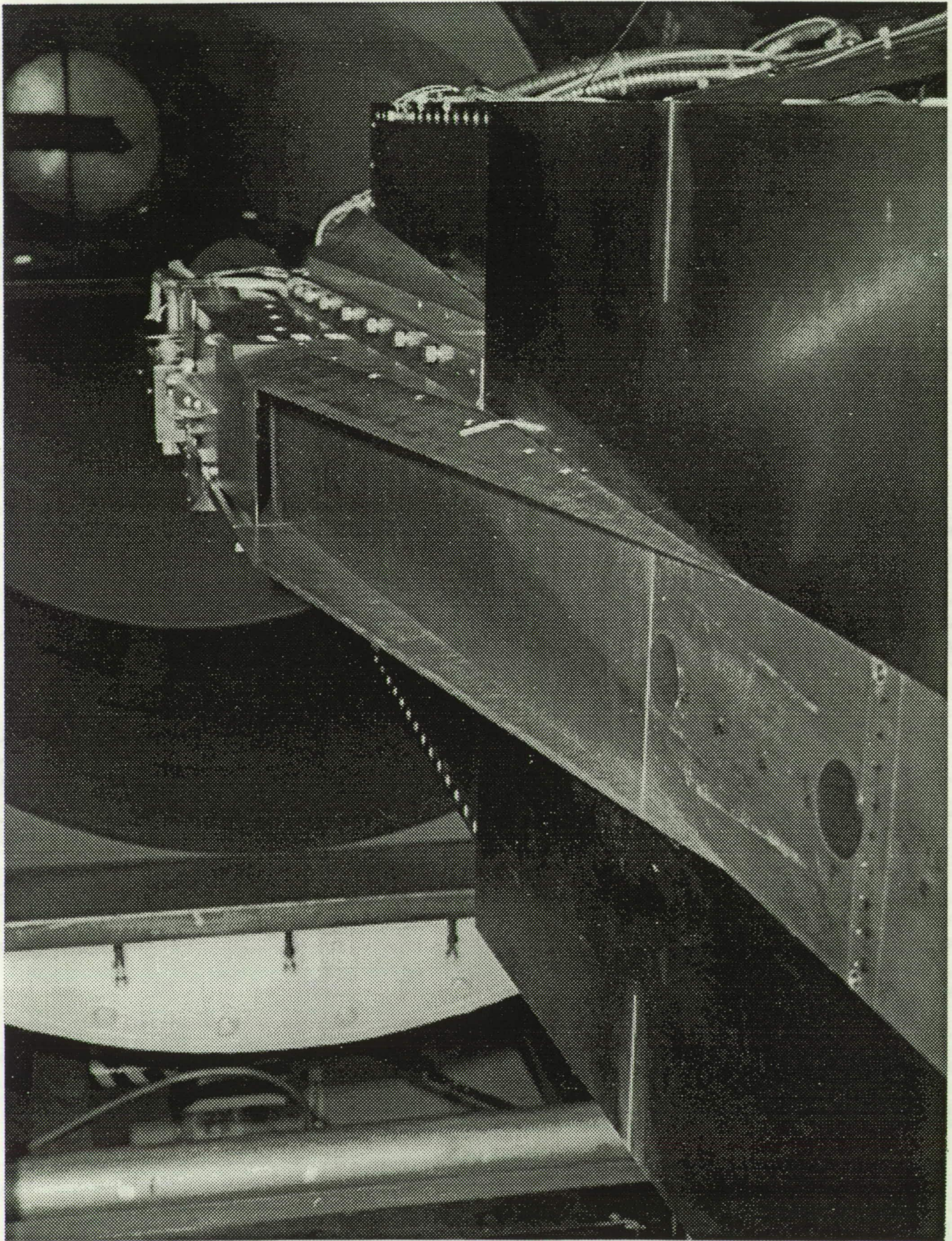
UNCLASSIFIED

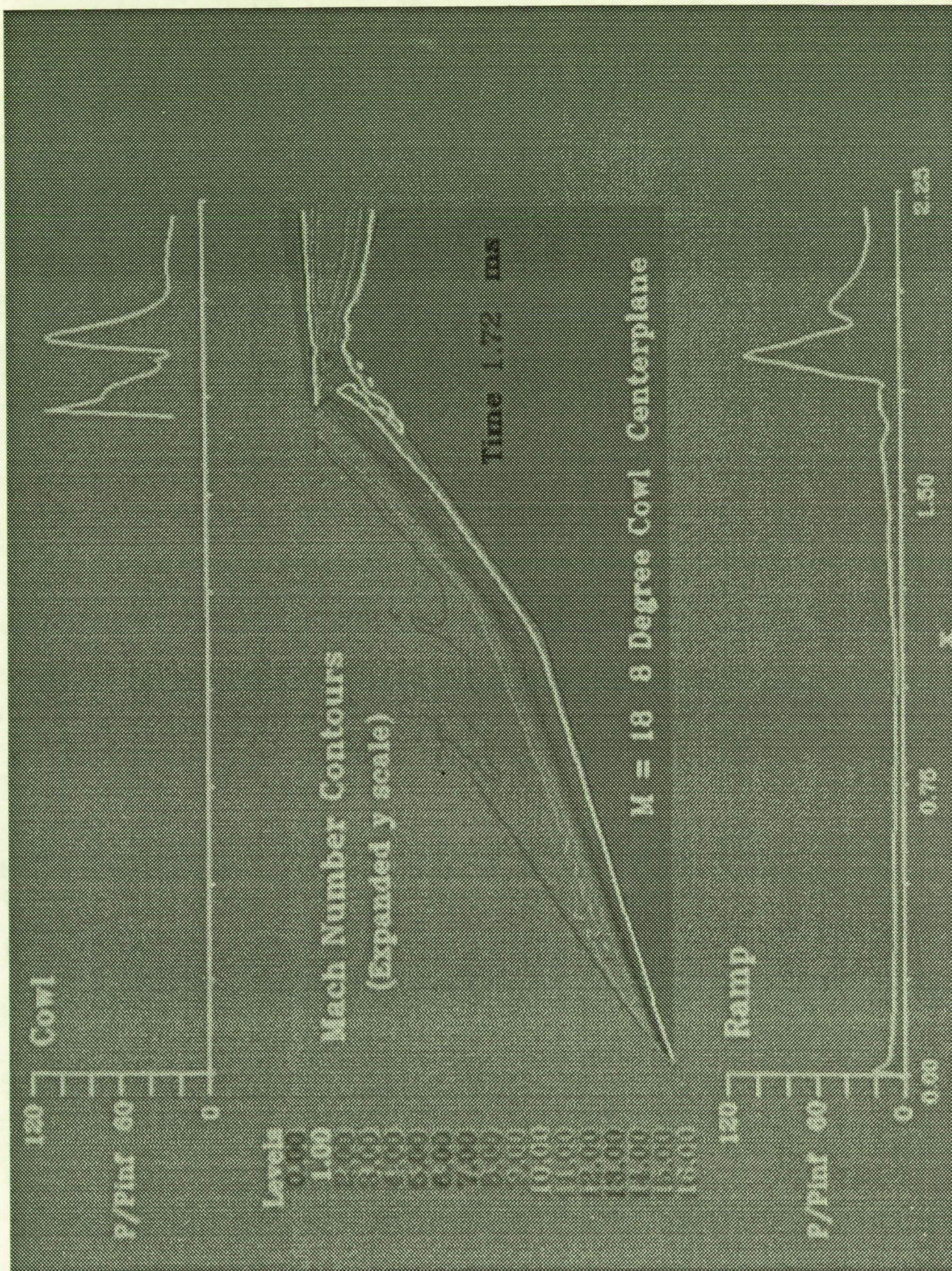
UNCLASSIFIED

45-11

91





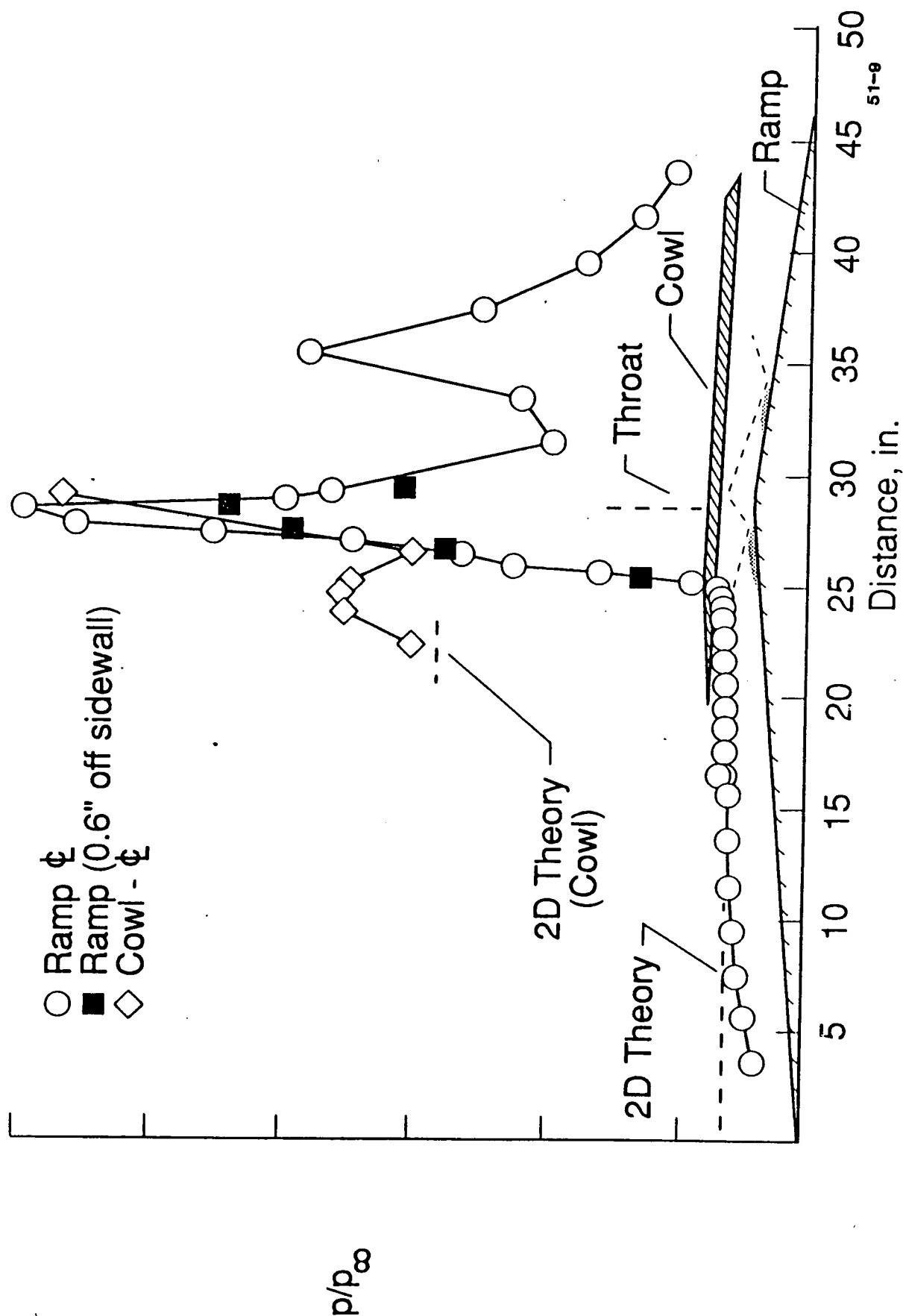


ORIGINAL PAGE
BLACK AND WHITE PHOTOGRAPH

41
ORIGINAL PAGE IS
OF POOR QUALITY

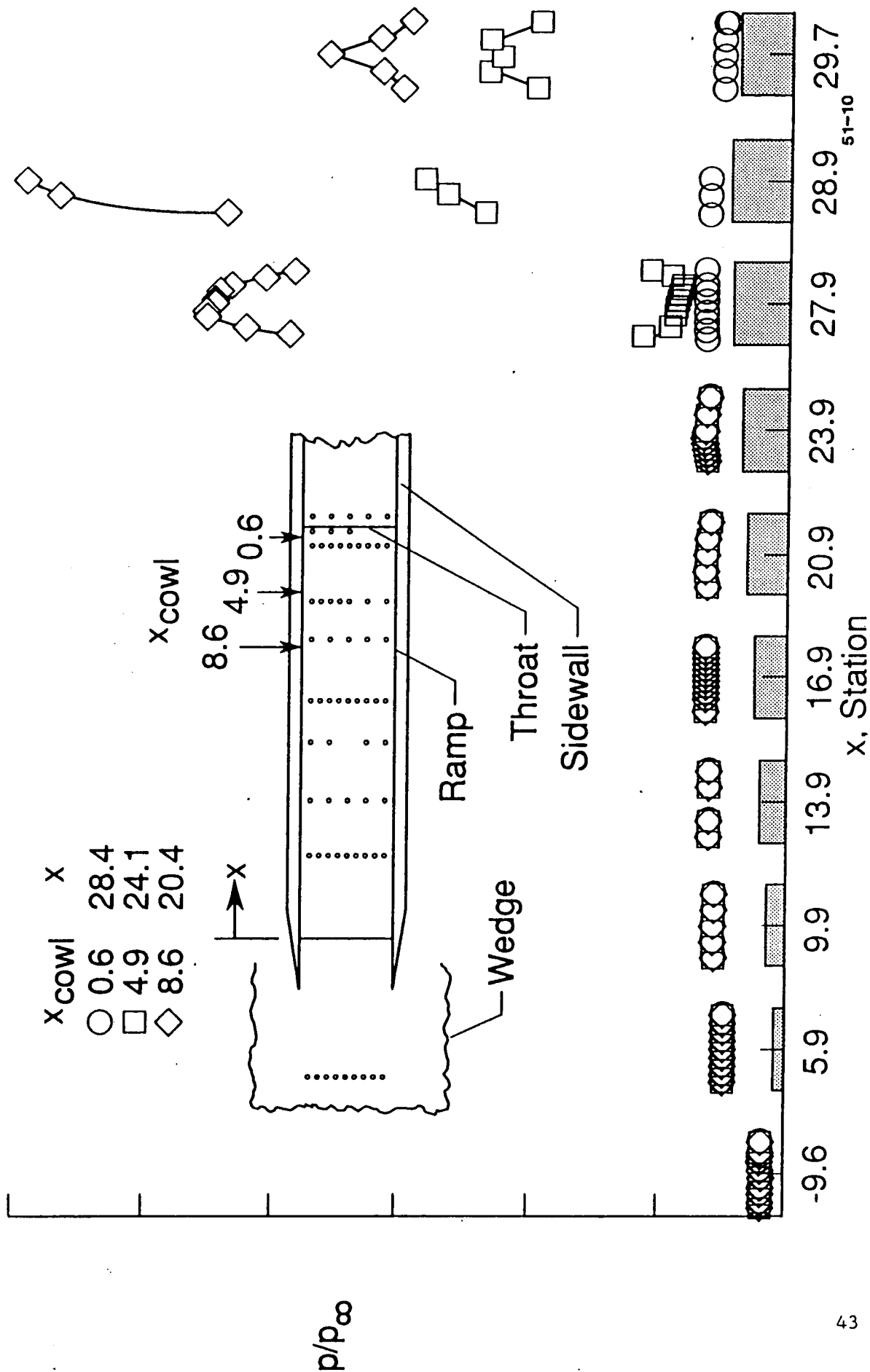
STATIC PRESSURE ON RAMP AND 8° COWL (U)

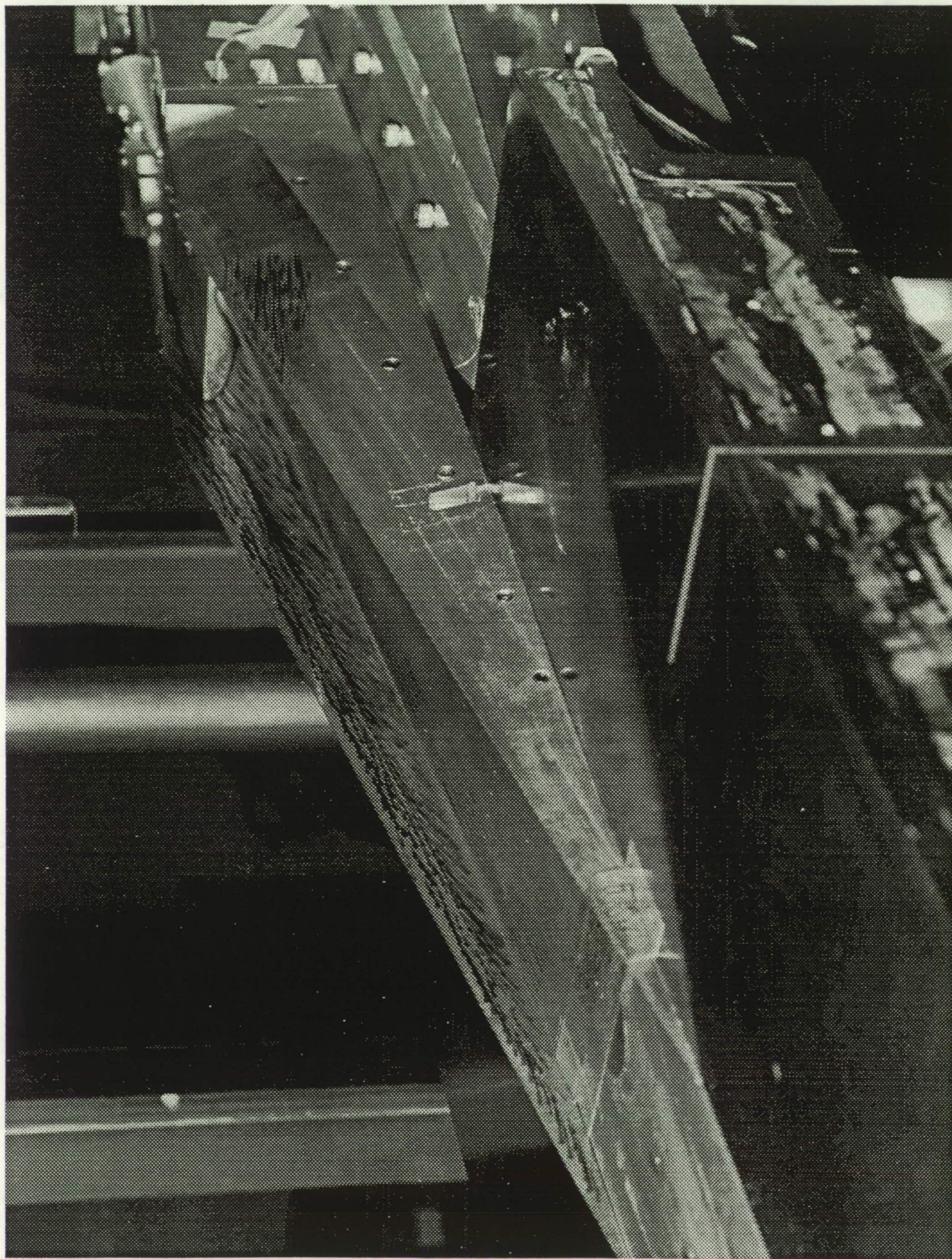
Mach 18, $P_T = 1200$ psia, $X_{cowl} = 8.6"$



PRESSURE VARIATION ACROSS WEDGE AND RAMP (U)

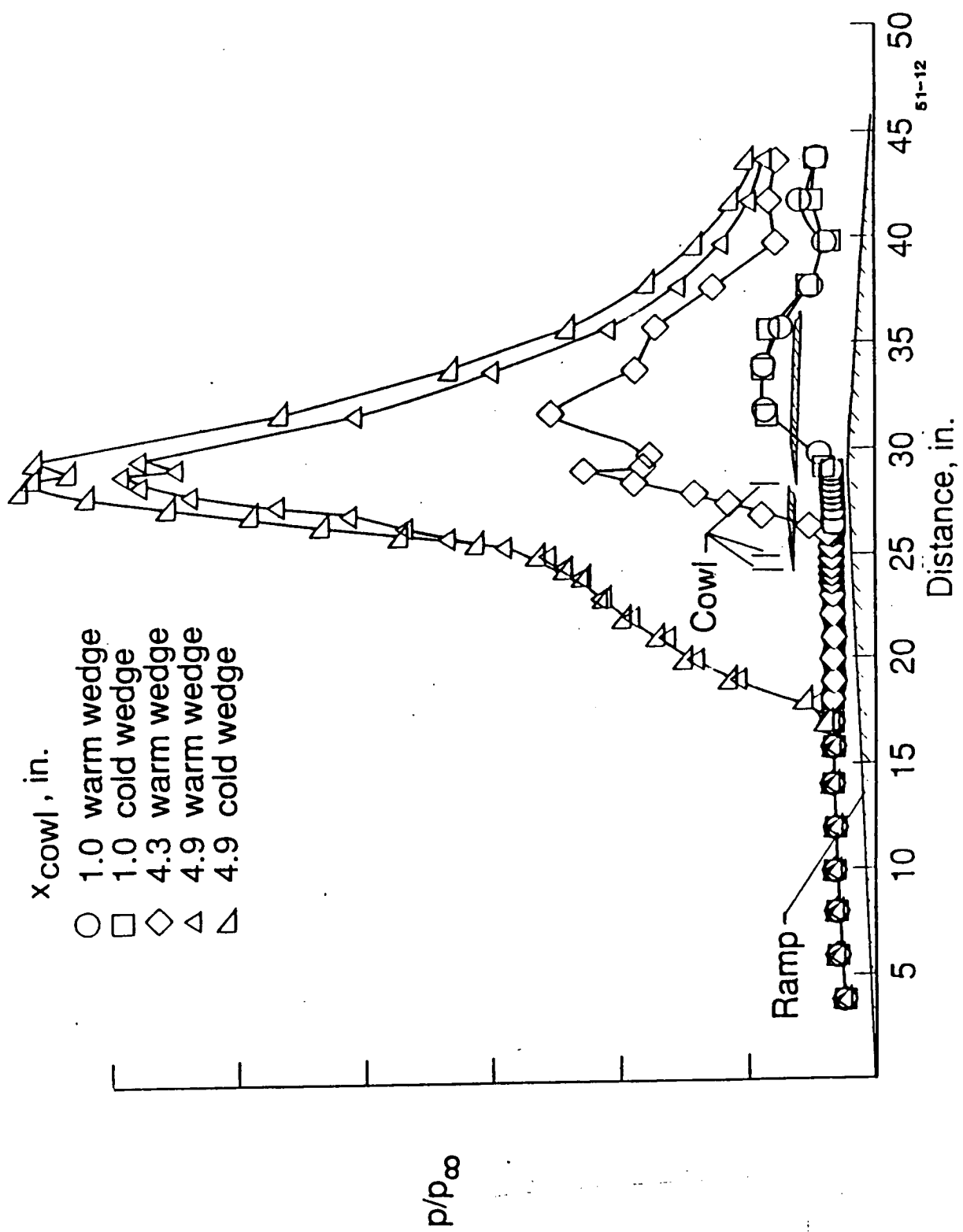
Mach 18, $P_T = 1200$ psia, 8° Cowl



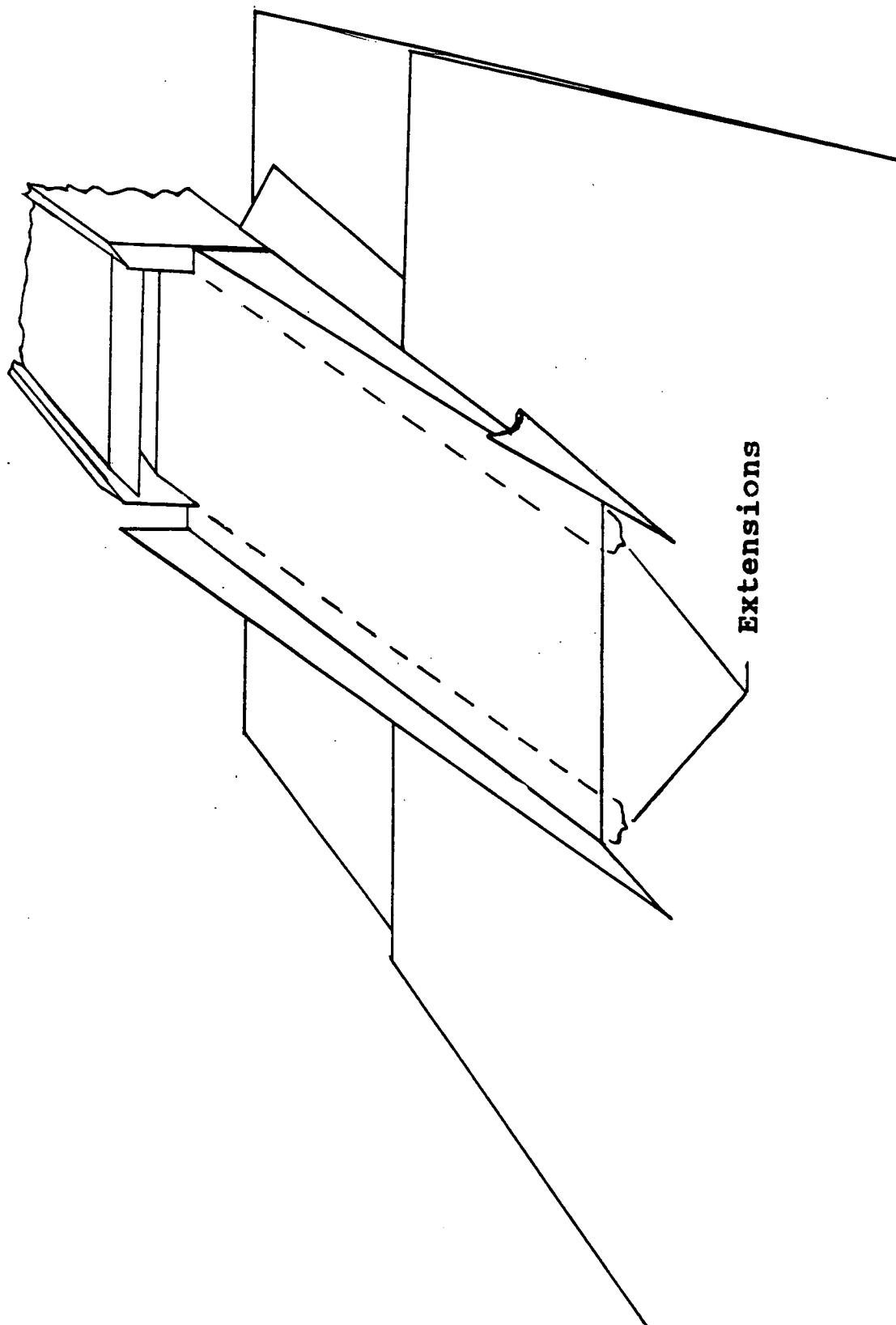


STATIC PRESSURE ON RAMP, 10° COWL (U)

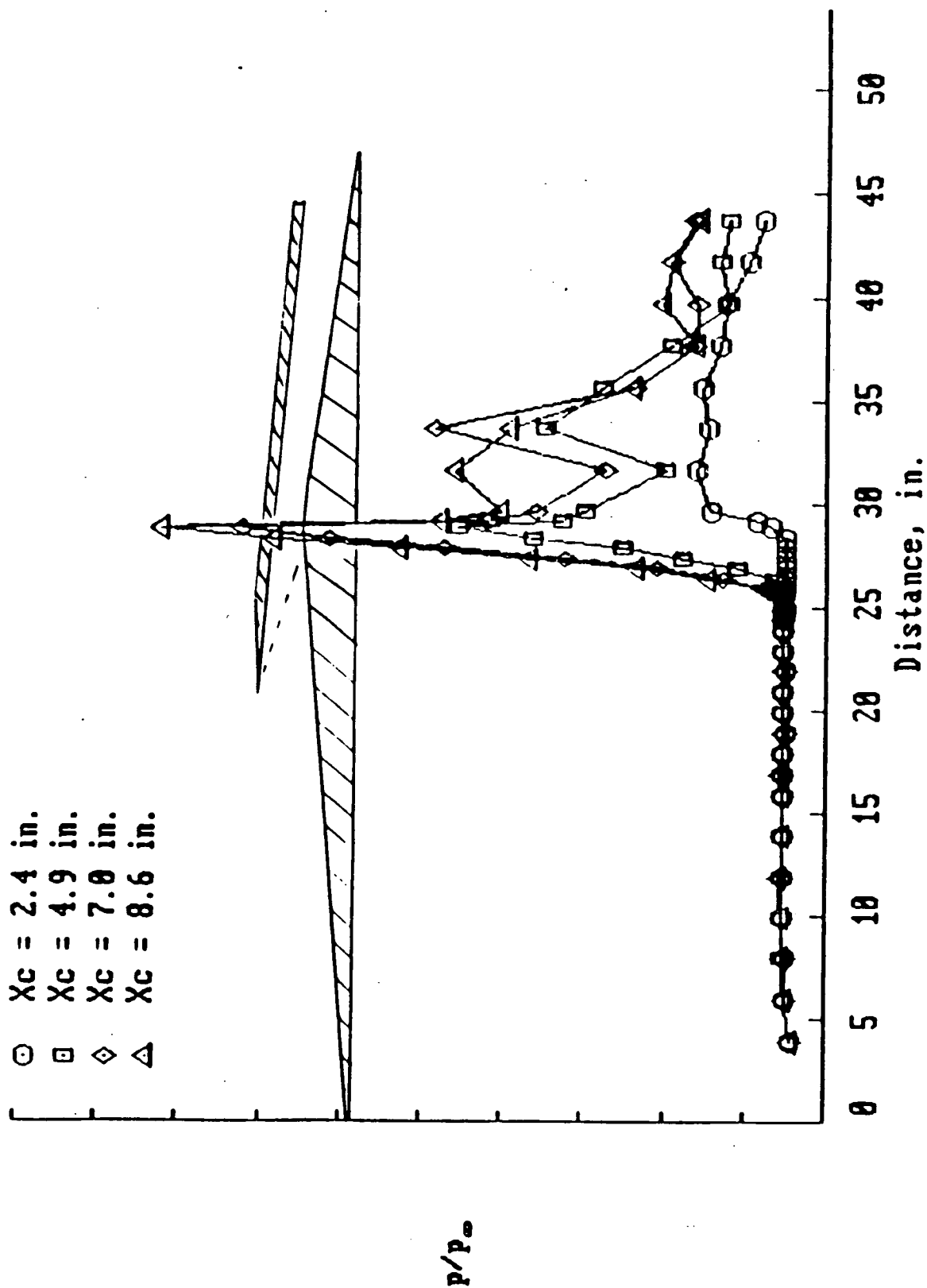
Mach 18, $P_T = 1200$ psia



RAMP EXTENSIONS



RAMP PRESSURE WITH 10° COWL & NO SIDEWALLS



CONCLUDING REMARKS

- Tests without a simulated forebody resulted in strong viscous interactions in the front portion of the inlet.
- With a simulated forebody, a more orderly inlet flow was noted, but still with significant bodyside viscous interactions.
 - Sidewall compression end effects on bodyside, sensitive to cowl location
 - 2-D inlet sidewall corner flow interaction with the cowl shock wave
- CFD analysis by Bill Rose and Ed Perkins tended to over predict viscous interactions
- Closer coordination with CFD community required to realize CFD code calibration aspects of high Mach number helium tests.